

**EE 323**  
**Analog circuits and Instrumentation**

**Midterm Examination**

November 3<sup>rd</sup>, 2006

Time: 2:30pm-3:50pm

Room: 1B79 Eng

84/100

5% Curve

Name: Shea Pederson

= 89%

Student number: 10288579

Answer all questions.  
State your assumptions if required.  
Calculator and 2 pages of formula are allowed.

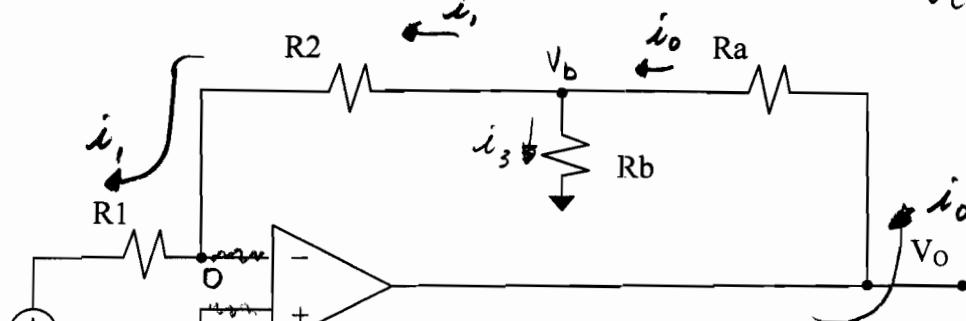
product  
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### Question 1:

The inverting amplifier below uses a feedback network in form of a "T-bridge" of  $R_a$ ,  $R_b$ , and  $R_2$ . Derive the transfer function of the amplifier  $V_o/V_i$  as a function of resistors  $R_1$ ,  $R_2$ ,  $R_a$ , and  $R_b$ . Assuming the op-amp is ideal.

Simplify  $V_o/V_i$  in the limits  $R_2 \gg R_b$  and  $R_2 \gg R_a$ .

$$\frac{V_o}{V_i}$$



$$i_1 = i_2$$

$$\frac{V_b}{R_2} = -\frac{V_i}{R_1}$$

$$V_i = -\frac{R_1}{R_2} V_b$$

$$-V_b = -\frac{R_2}{R_1} V_i$$

$$\frac{V_o - V_b}{R_a} = \frac{V_b}{R_b} + i_1$$

$$\frac{V_o}{R_a} = \frac{V_b}{R_b} + \frac{V_b}{R_a} + \frac{V_b}{R_2}$$

$$V_o = V_b \left( \frac{1}{R_b} + \frac{1}{R_a} + \frac{1}{R_2} \right) R_a$$

$$V_o = -\frac{R_2}{R_1} V_i \left( \frac{R_a}{R_b} + 1 + \frac{R_a}{R_2} \right)$$

$$\frac{V_o}{V_i} = -\frac{R_2 R_a}{R_1} \left( \frac{R_a R_2 + R_b R_2 + R_b R_a}{R_b R_a R_2} \right)$$

$$\boxed{\frac{V_o}{V_i} = -\left( \frac{R_a R_2 + R_b R_2 + R_b R_a}{R_1 R_b} \right)}$$

$$\lim_{R_2 \gg R_b} \frac{V_o}{V_i} = -\left( \frac{R_a R_2 + R_b R_2}{R_1 R_b} \right) = -R_2 \left( \frac{R_a + R_b}{R_1 R_b} \right)$$

$$\lim_{R_2 \gg R_a} \frac{V_o}{V_i} = -\left( \frac{R_2 R_a + R_2 R_b}{R_1 R_b} \right) = -R_2 \left( \frac{R_a + R_b}{R_1 R_b} \right)$$

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simply neglect  $R_a R_b$

## Question 2:

Find the expression of the output voltage  $V_Z$  with respect to the input voltages  $V_1$  and  $V_2$ .

It has been known that the current through a diode is:  $I_D \approx I_S e^{(V_D/\eta V_T)}$  where  $V_D = \text{diode voltage}$ ,  $I_S = 10^{-12} \text{ A}$ ,  $V_T = 25 \text{ mV}$ ,  $\eta = 1.5$ .

$$I_D \approx I_S e^{\left(\frac{V_D}{\eta V_T}\right)} \approx 10^{-12} (e^{\frac{V_D}{\eta V_T}}) V_D$$

$$I_D \approx 10^{-12} (381 \cdot 10^9) V_D$$

Find  
 $V_Z(V_1, V_2)$

$$\boxed{\text{Find } \frac{V_X}{V_1} = G_d}$$

$$V_X = -V_D$$

$$\frac{V_1}{R_1} = I_D \quad \checkmark$$

then  $I_D = I_S e^{\frac{V_D}{\eta V_T}}$

$$\frac{V_1}{R_1} = 10^{-12} (381 \cdot 10^9)^{-V_X}$$

$$\frac{V_1 \cdot 10^{12}}{R_1} = 381 \cdot 10^9 e^{-V_X}$$

couldn't find  
assume  $G_d = \frac{V_X}{V_1} = \frac{V_Y}{V_2}$

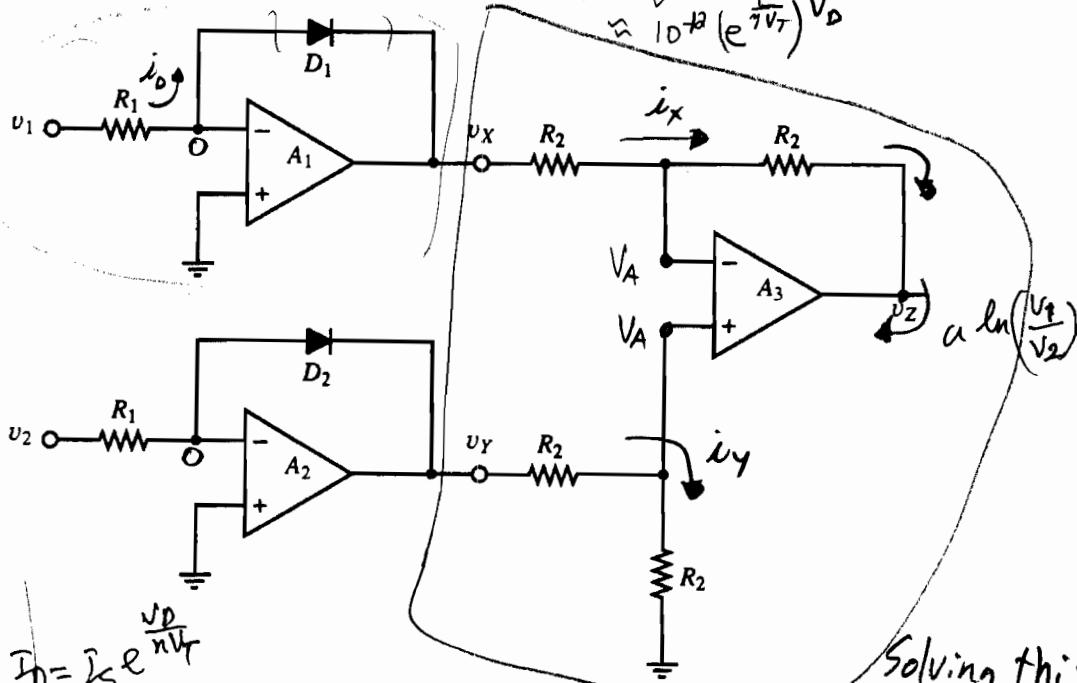
$$V_X = G_d V_1$$

$$V_Y = G_d V_2$$

$$\boxed{V_Z = G_d (V_2 - V_1)}$$

$$\text{where } G_d = \frac{V_X}{V_1} = \frac{V_Y}{V_2}$$

looks like a differential amplifier.  $\times$



Solving this:

$$V_A = \frac{1}{2} V_Y$$

$$\frac{V_X - V_A}{R_2} = \frac{V_A - V_Z}{R_2}$$

$$V_X = 2V_A - V_Z$$

$$V_X = 2 \cdot \frac{1}{2} V_Y - V_Z$$

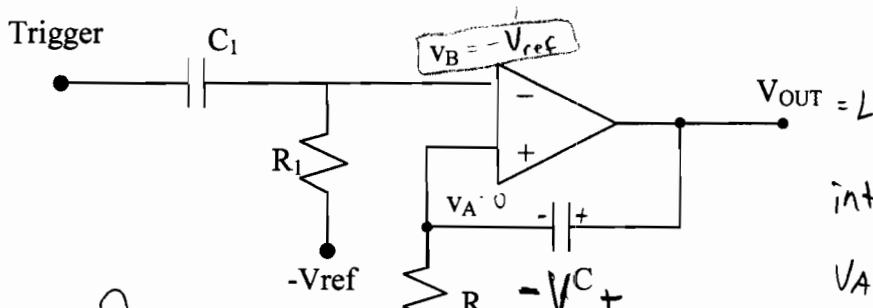
$$V_X = V_Y - V_Z$$

$$\boxed{V_Z = V_Y - V_X}$$

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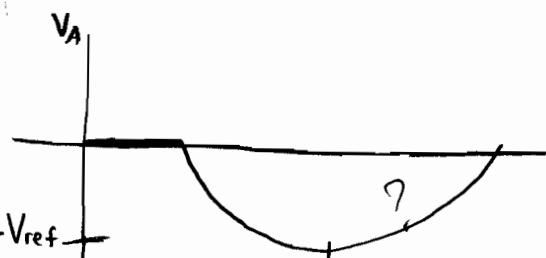
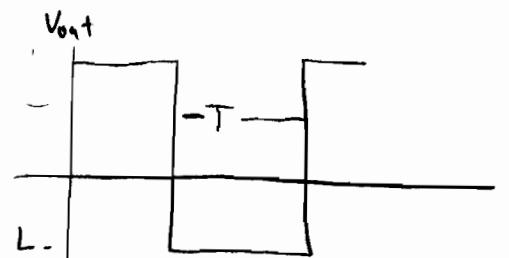
### Question 3:

The circuit below is a monostable multivibrator. In the stable state, the output  $V_{OUT} = L_+$ ,  $v_A = 0$  and  $v_B = -V_{ref}$ . The circuit can be triggered by applying a positive input pulse of height greater than  $V_{ref}$ . For normal operation,  $C_1 R_1 \ll CR$ . Show the resulting waveforms of  $V_{OUT}$  and  $v_A$ . Find the width of the output pulse  $T$ . (i.e.,  $T$  is a function of  $C$ ,  $R$ ,  $L_+$ ,  $L_-$ , and  $V_{ref}$ ).

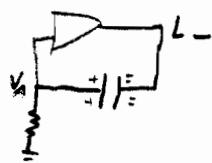


$$\beta(s) = \frac{V_A}{V_{out}} = \frac{R}{R + \frac{1}{Cs}} = \frac{Rcs}{Rcs + 1}$$

$$V_A = \beta V_{out},$$



After trigger:



-30

$$V_c = L_- - (L_- - L_+) e^{-t/RC}$$

$$V_A = V_{out} - V_c$$

After trigger (sends  $V_{out}$  to  $L_-$ ) -15-15

$$V_A = L_- - V_c$$

$$V_A = (L_- - L_+) e^{-t/RC}$$

The opamp will flip again to  $L_+$  when  $V_A > -V_{ref}$ . This is the period,  $t = T$

$$-V_{ref} = (L_- - L_+) e^{-T/RC}$$

$$\frac{-V_{ref}}{L_- - L_+} = e^{-T/RC}$$

$$\ln\left(\frac{-V_{ref}}{L_- - L_+}\right) = \frac{-T}{RC}$$

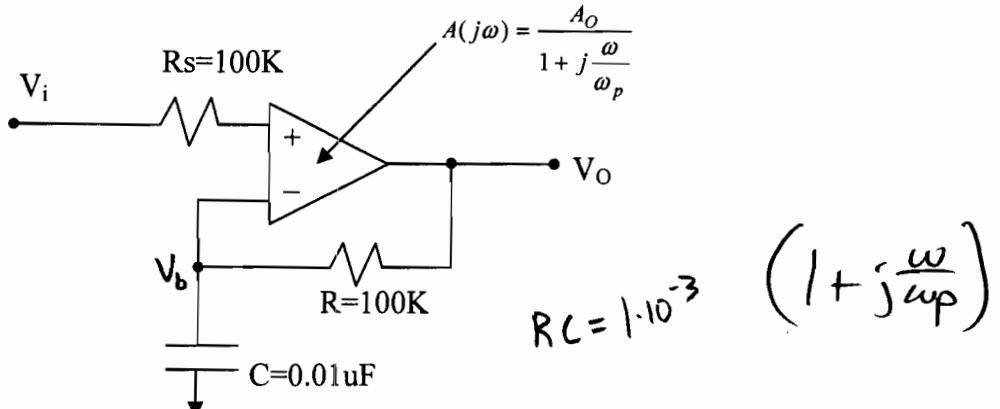
$$T = RC \ln\left(\frac{-V_{ref}}{L_- - L_+}\right)$$

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**Question 4:**

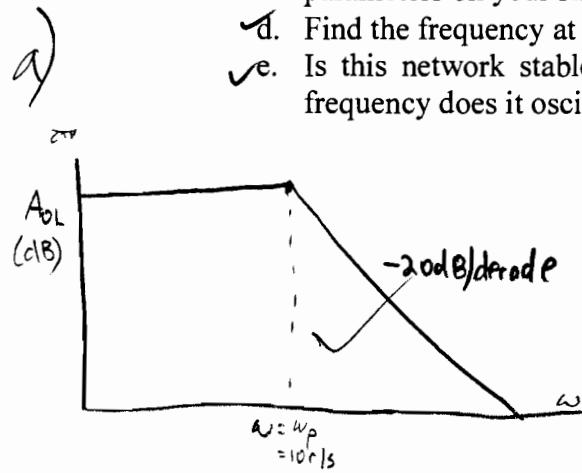
$$A_{OL} = A = 10^5$$

The op-amp in the circuit below has an open-loop gain of  $10^5$  and a single pole with  $\omega_p = 10\text{ rad/s}$ .



- ✓ a. Sketch the open-loop Bode plot.
- b. The gain equation for this non-inverting amplifier with negative feedback is in the form:  

$$\frac{V_o}{V_i} = \frac{A(j\omega)}{1 + A(j\omega)\beta(j\omega)}$$
 where  $\beta(j\omega)$  is the negative feedback factor. Find this closed-loop transfer function, including its poles and zero.
- ✓ c. Sketch the magnitude of the transfer function (gain) versus frequency and label important parameters on your sketch.
- ✓ d. Find the frequency at which  $|A\beta|=1$ .
- ✓ e. Is this network stable or it will oscillate at certain frequency? If it is unstable, what frequency does it oscillate?



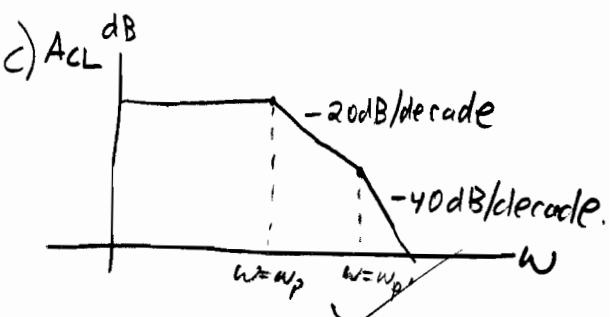
$$\beta(j\omega) = \frac{V_o}{V_i} = \frac{\frac{1}{Cs}}{\frac{1}{Cs} + R} = \frac{1}{1 + RCs} = \frac{1}{1 + RCL\omega} \quad \checkmark$$

$$\begin{aligned} A_{CL}(j\omega) &= \frac{\frac{A_0}{1 + j\frac{\omega}{\omega_p}}}{1 + \frac{A_0}{1 + j\frac{\omega}{\omega_p}} \cdot \frac{1}{1 + RCL\omega}} = \frac{A_0}{1 + j\frac{\omega}{10} + \frac{A_0}{1 + RCL\omega}} \\ &= \frac{A_0(1 + RCL\omega)}{1 + RCL\omega + j\frac{\omega}{10}(1 + RCL\omega) + A_0} = \end{aligned}$$

$$= A_0 \frac{(1 + RCL\omega)}{1 + RCL\omega + j\frac{\omega}{10} - \frac{\omega^2}{10}RC + A_0} \quad \checkmark$$

$$= \frac{A_0 + A_0 RCL\omega}{1 - \frac{\omega^2}{10}RC + A_0 + j(RCL\omega + \frac{\omega}{10})} \quad \checkmark$$

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d) Find  $f$  when  $A\beta = 1$

$$\left| L(s) \right| = 1 = \left| \frac{10^5}{1 + j \frac{\omega}{10}} \cdot \frac{1}{1 + RCj\omega} \right|$$

$$1 = \left| 10^5 \cdot \frac{1}{(1 + j \frac{\omega}{10})(1 + 10^{-3}j\omega)} \right|$$

Solve via MP

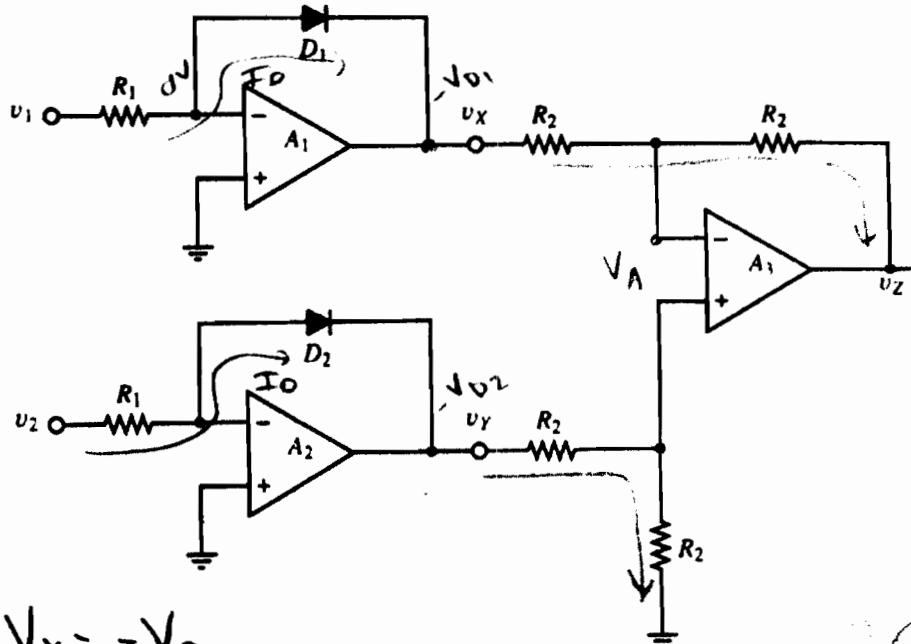
$$\omega = 31615 \text{ rad/s} \quad \cancel{\text{so}} \quad f = \frac{\omega}{2\pi}$$

$$f = 5.03 \text{ kHz} \quad \checkmark$$

e) It is unstable (oscillator) with an oscillating frequency of 5.03 kHz.  $\times$

## Question 2:

Find the expression of the output voltage  $V_Z$  with respect to the input voltages  $V_1$  and  $V_2$ . It has been known that the current through a diode is:  $I_D \approx I_s \exp(V_D/nV_T)$  where  $V_D$  = diode voltage,  $I_s = 10^{-12} A$ ,  $V_T = 25 mV$ ,  $n=1.5$ .



$$V_x = -V_{D1}, \quad V_y = -V_{D2}$$

$$\frac{V_x - V_A}{R_2} = \frac{V_A - V_2}{R_2} \Rightarrow 2V_A = V_x + V_2$$

$$V_A = \frac{V_x + V_2}{2}$$

$$\frac{V_y - V_A}{R_2} = \frac{V_A - V_1}{R_2} \Rightarrow V_A = \frac{V_1 + V_2}{2}$$

$$V_x + V_2 = V_y$$

$$V_x - V_y = -V_2$$

$$\textcircled{1} \Rightarrow V_2 = V_y - V_x$$

$$I_D = \frac{V_1}{R_1} \Rightarrow \frac{V_1}{R_1} = I_s \exp(V_D/nV_T) \Rightarrow \text{Solve for } V_D \Rightarrow \ln \frac{V_1}{R_1 I_s} = \frac{V_D}{nV_T}$$

$$V_{D1} = nV_T \ln \left( \frac{V_1}{R_1 I_s} \right) \textcircled{2} \quad V_{D2} = nV_T \ln \left( \frac{V_2}{R_1 I_s} \right) \textcircled{3}$$

①, ②, ③

$$V_2 = V_y - V_x = -nV_T \ln \left( \frac{V_1}{R_1 I_s} \right) = nV_T \left( \ln V_1 - \ln R_1 I_s - \ln V_2 + \ln R_1 I_s \right)$$